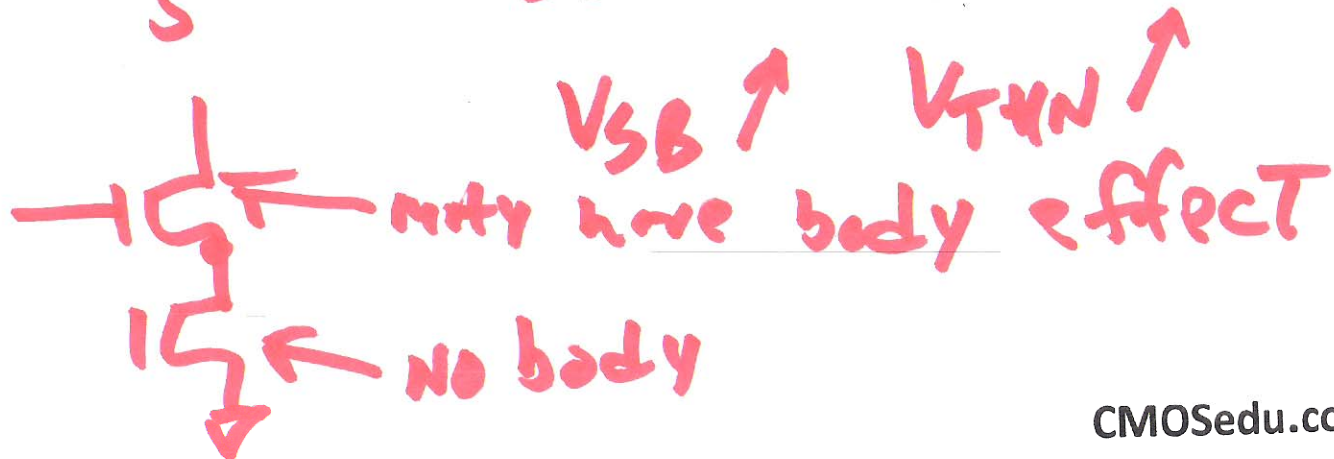
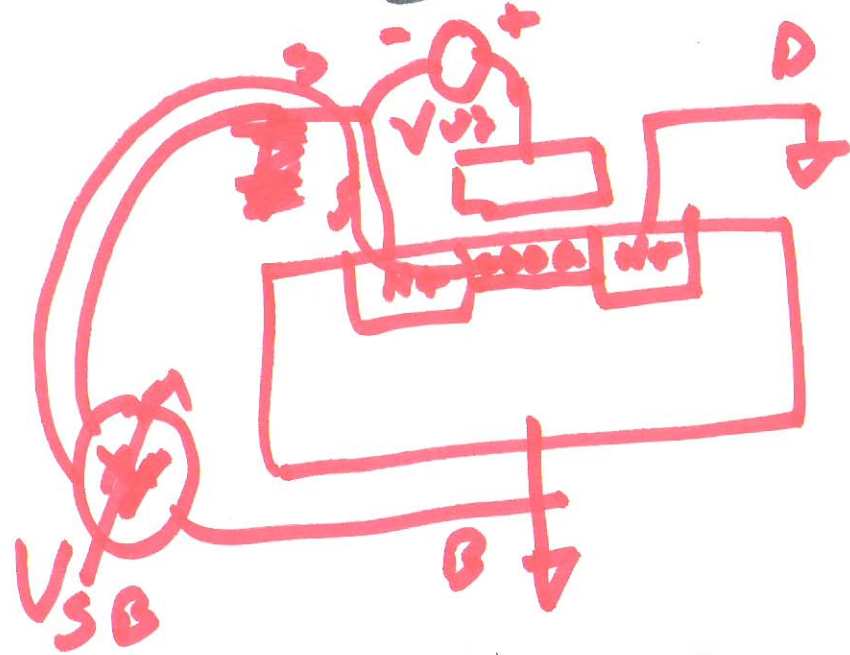
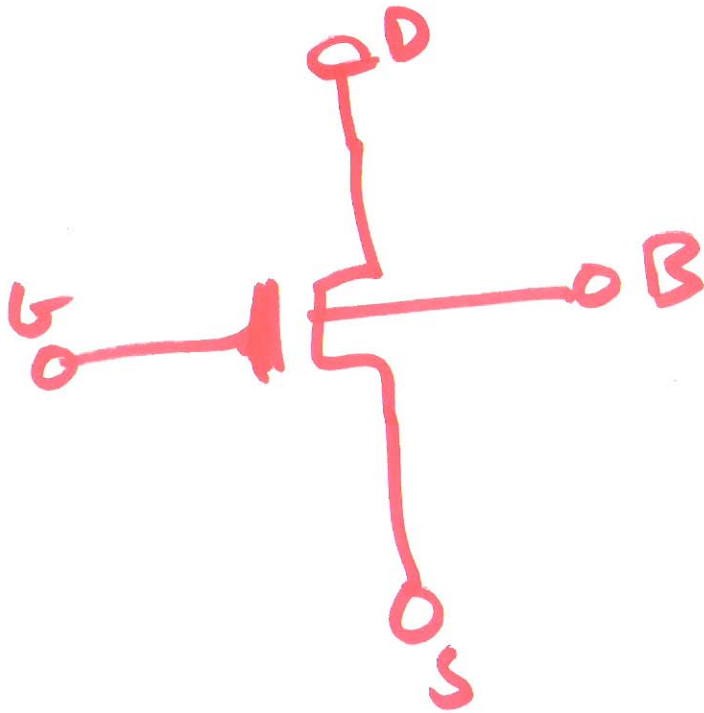


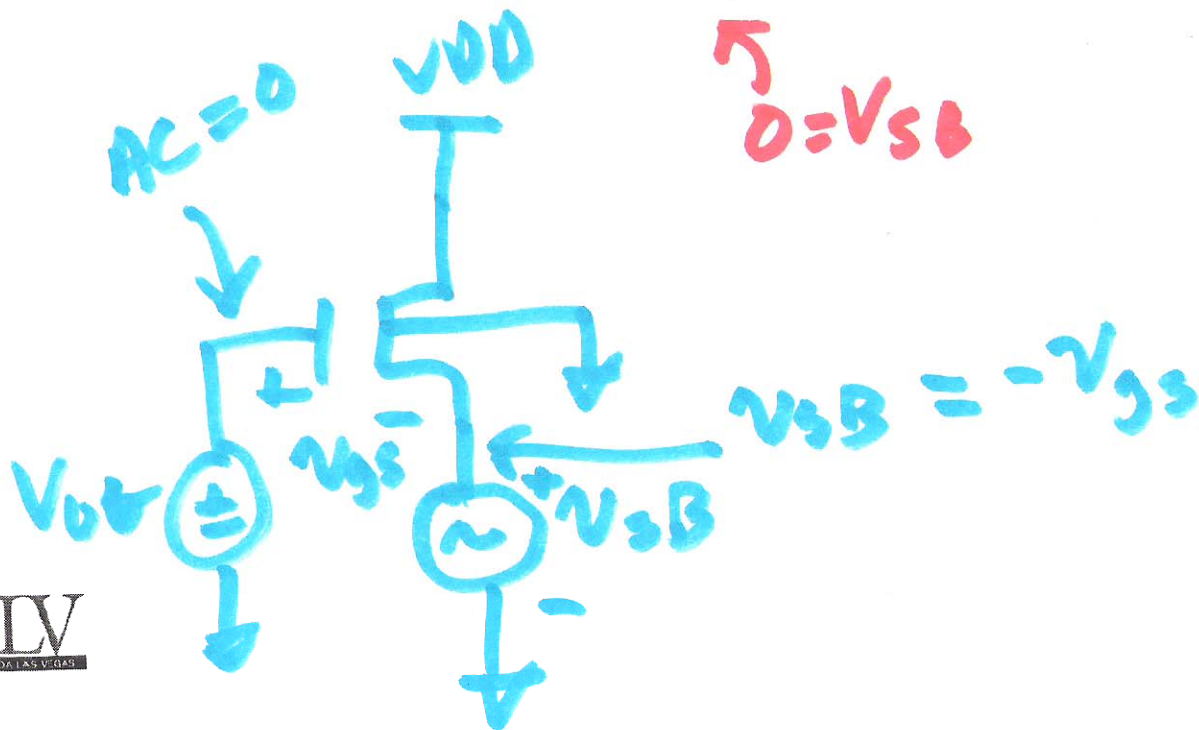
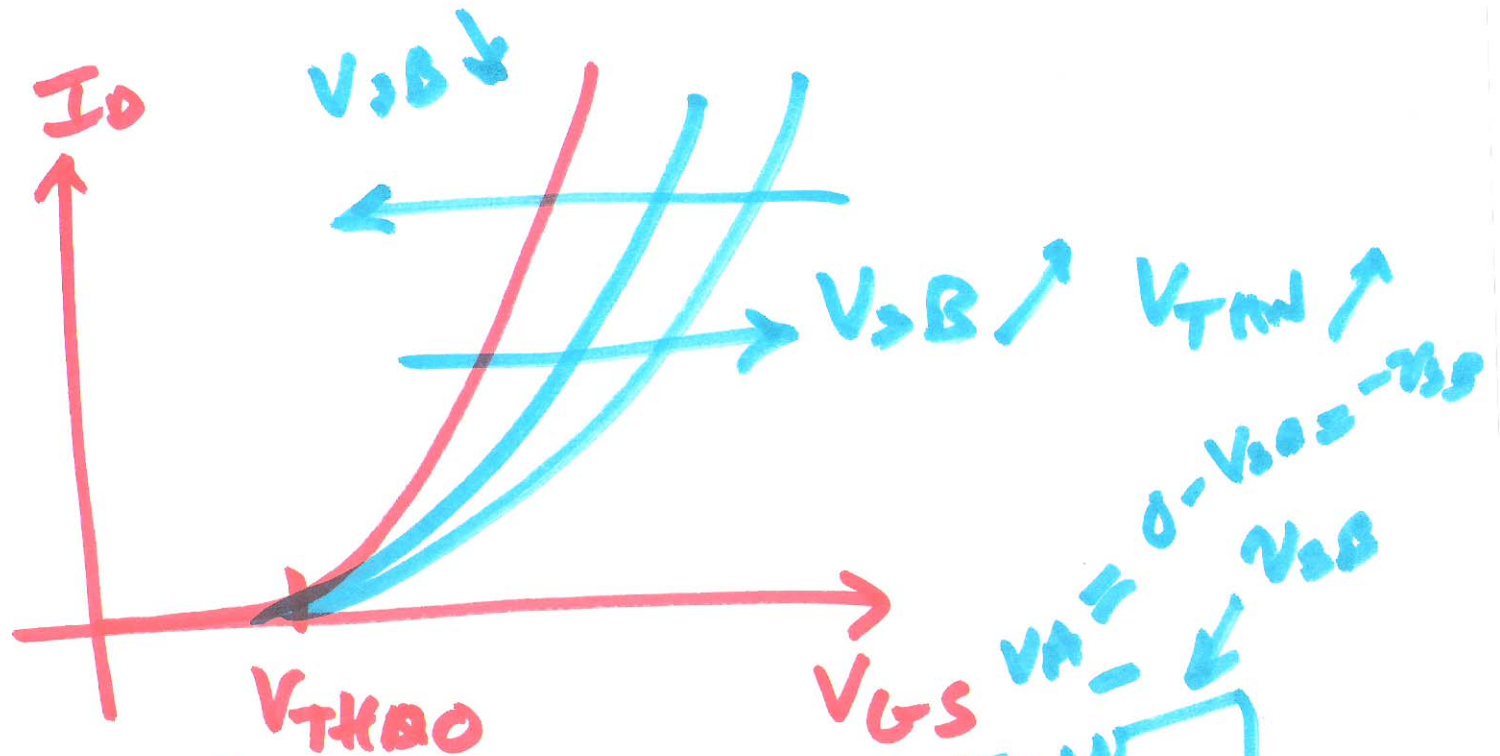
EE 420 / ECG 620

Analog

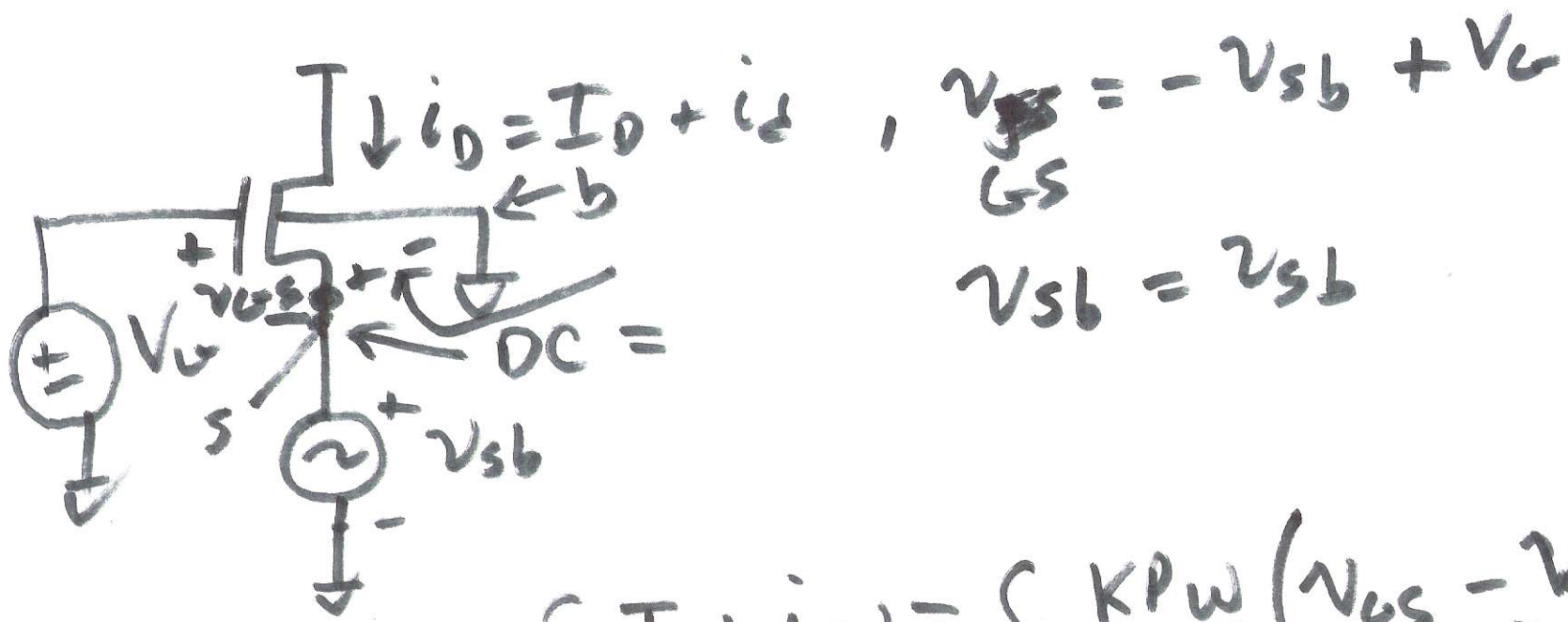
1/29/14

Lecture 3





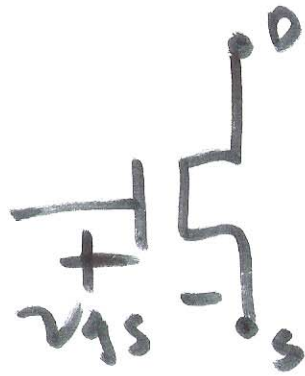
2)



$$\frac{\int (I_D + i_d)}{\int v_{sb}} = \frac{\int \frac{K_P W}{2 L} (V_{GS} - V_{THN})^2}{\int v_{sb}}$$

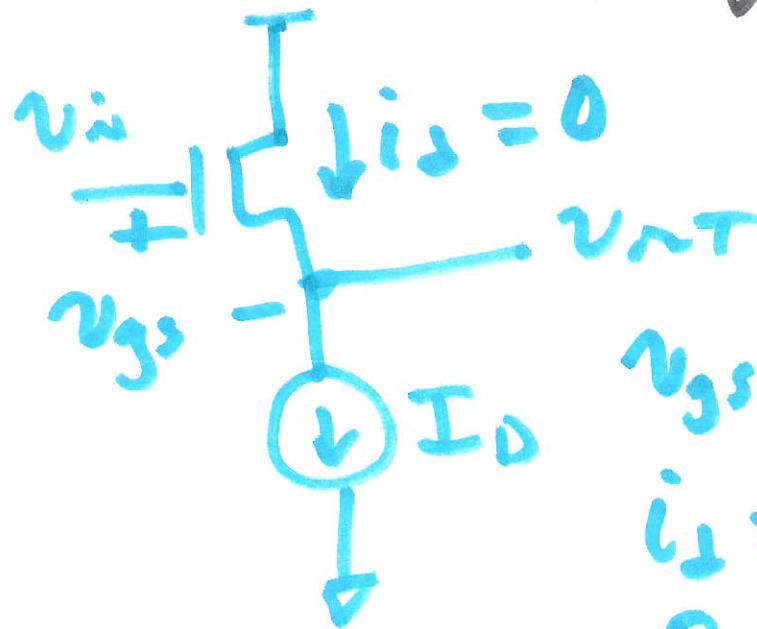
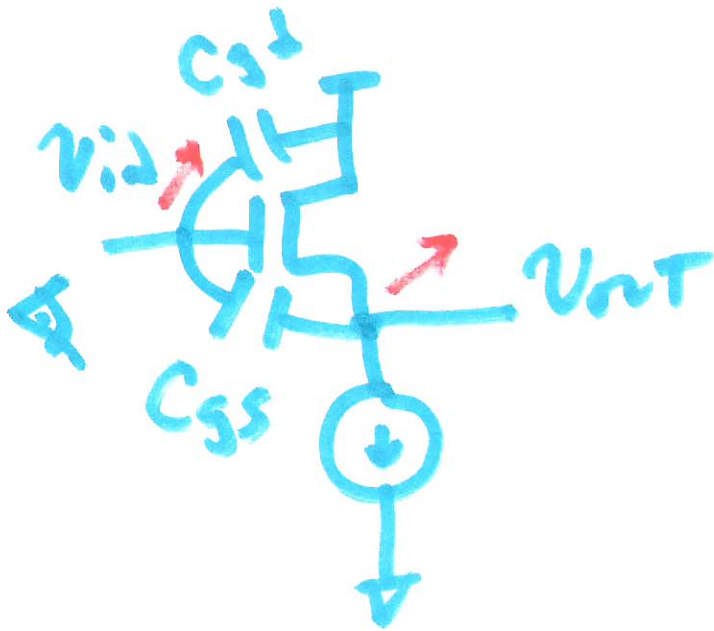
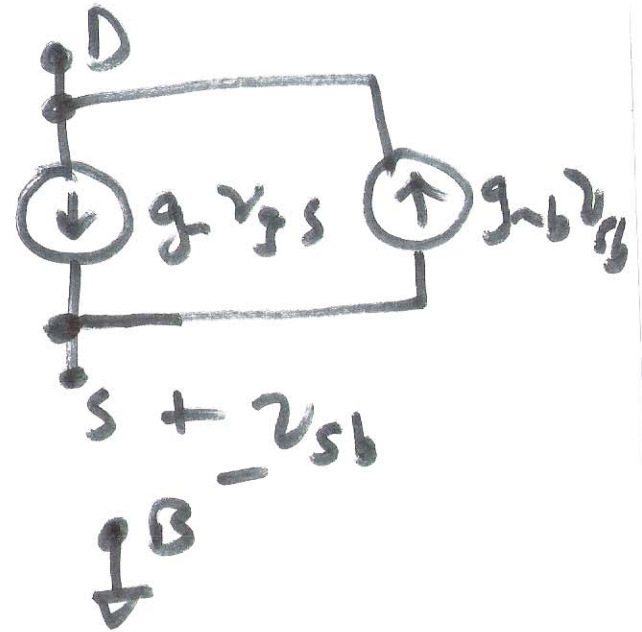
$i_d = g_{mb} \cdot v_{sb}$

$I_D = \text{const}$   
 $V_{GS} = \text{const}$



$$i_d = g_m v_{gs} - g_{mb} v_{sb}$$

SF → source follower



No body effect

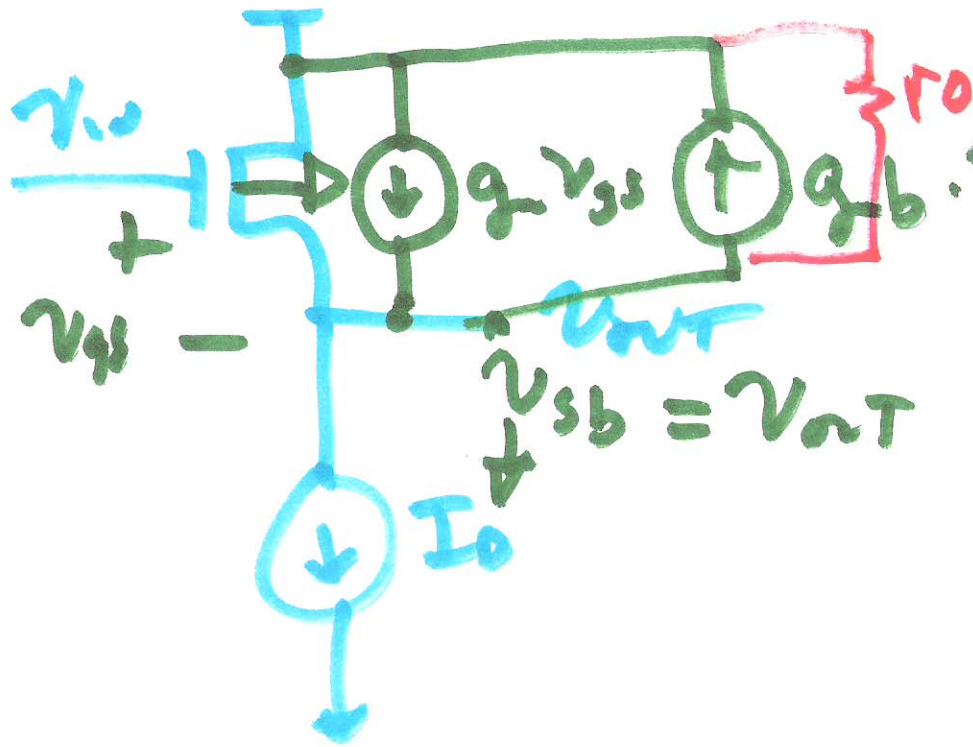
$$v_{gs} = v_{id} - v_{out}$$

$$i_d = g_m v_{gs}$$

$$0 = g_m (v_{id} - v_{out})$$

$$v_{id} = v_{out}$$

$$v_{out}/v_{id} = 1$$



$$v_{gs} = v_{in} - v_{out}$$

$$g_m v_{gs} = g_b (v_{out})$$

$$g_m v_{in} - g_m v_{out} = g_b v_{out}$$

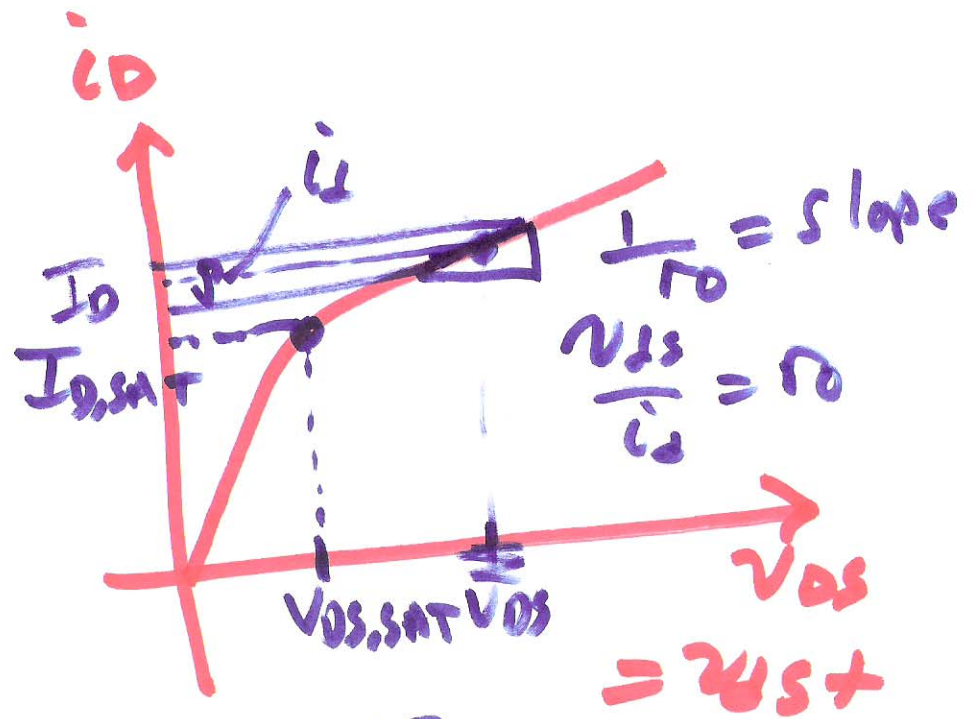
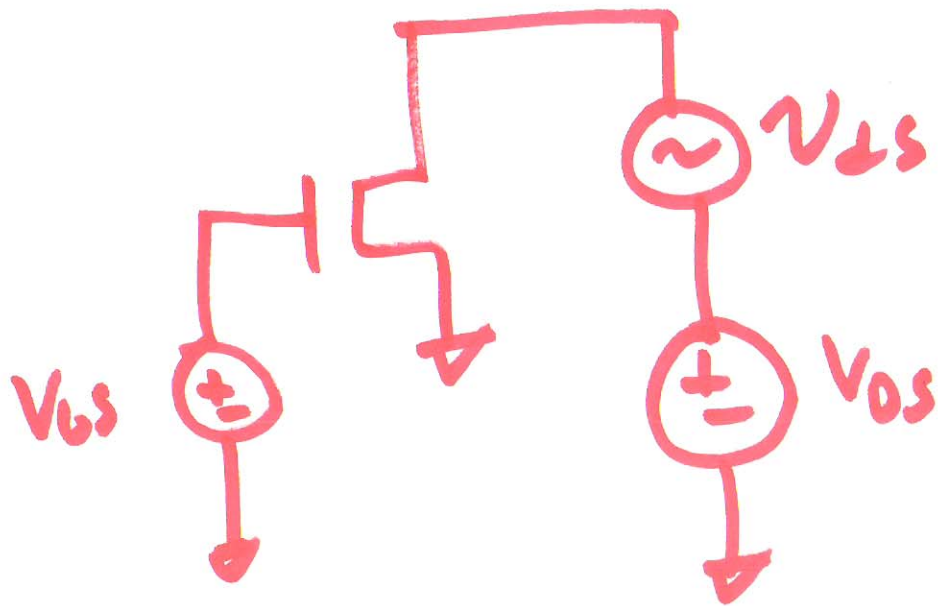
$$g_m v_{in} = v_{out} (g_m + g_b)$$

$$\frac{v_{out}}{v_{in}} = \frac{g_m}{g_m + g_b}$$

$$g_b = 0.4 g_m$$

$$\underline{\underline{.71 \approx \frac{1}{1.4}}}$$

5)



$$I_{D,SAT} = \frac{K_P}{2} \frac{W}{L} (V_{GS} - V_{THN})^2 = \frac{K_P}{2} \frac{W}{L} V_{DS,SAT}^2$$

$$V_{DS,SAT} = V_{GS} - V_{THN}$$

$$I_D = I_{D,SAT} (1 + \lambda (V_{DS} - V_{DS,SAT}))$$

$$V_{DS} \geq V_{DS,SAT}$$

6)

$$\frac{1}{r_o} = \left. \frac{\delta i_d + I_D}{\delta v_{DS}} \right|_{\substack{I_D = \text{CONST} \\ v_{DS} = \text{CONST}}} = \frac{\delta}{\delta v_{DS}} \left( I_{D,SAT} (1 + \lambda (v_{DS} + v_{DS} - v_{DS,SAT})) \right)$$

$$= I_{D,SAT} \lambda \left( \frac{v_{DS} + v_{DS}}{v_{DS}} - \cancel{v_{DS,SAT}} \right)$$

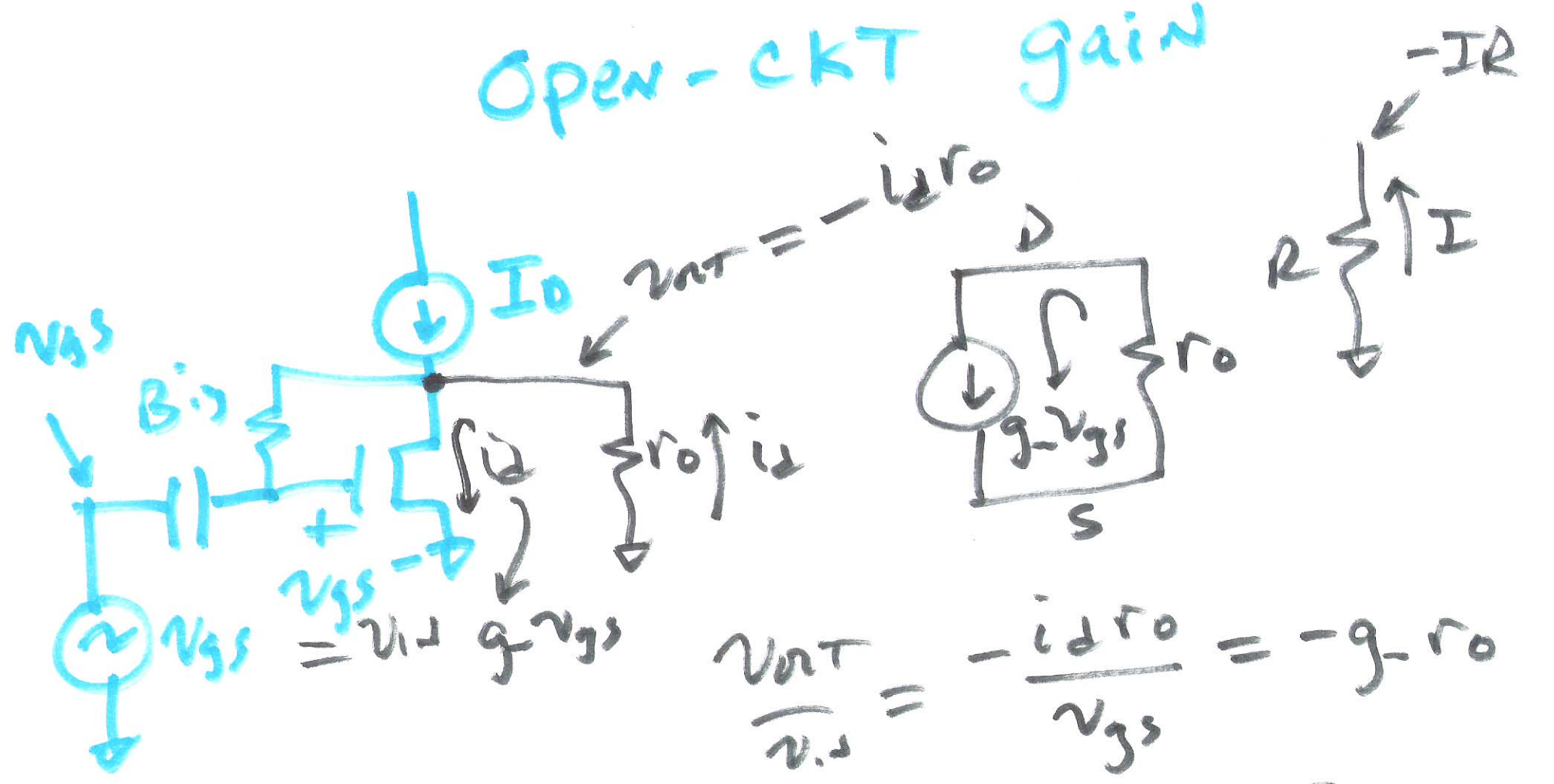
$v_{DS} \gg v_{DS,SAT}$

$$\frac{1}{r_o} = \lambda I_{D,SAT}$$

$$r_o = \frac{1}{\lambda I_{D,SAT}}$$

7)

# Open-ckt gain



$$v_{out} = -i_d r_o$$

$$\frac{v_{out}}{v_{gs}} = \frac{-i_d r_o}{v_{gs}} = -g_m r_o$$

$$|open\ ckt| = \boxed{g_m r_o}$$

8)



$$g_m r_o = \sqrt{2k_p \frac{W}{L} \cdot I_D} \cdot \frac{1}{\lambda I_D}$$

$$g_m r_o \propto \frac{1}{\sqrt{I_D}}$$

$I_D \uparrow$  gain,  $g_m r_o \downarrow$

for subthreshold  $g_m = \frac{I_D}{n \cdot V_T}$

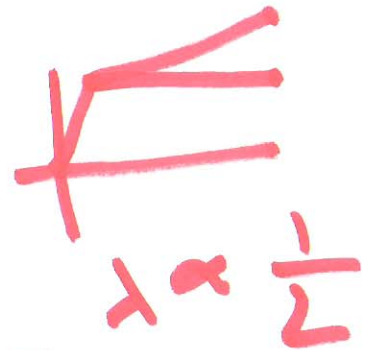
$g_m r_o$  independent of  $I_D$

Thermal  
voltage  
.026-V  
 $\frac{kT}{q}$

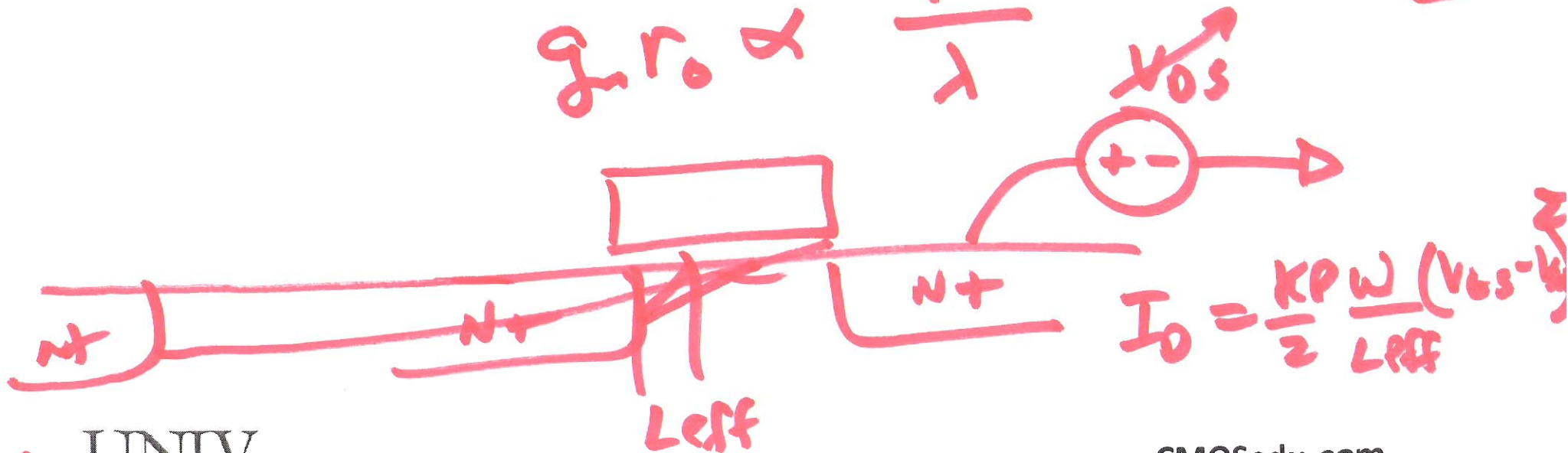
$$g_m r_o = \sqrt{2 K_P \frac{W}{L} \cdot I_0} \cdot \frac{1}{\lambda \cdot \frac{K_P W}{2 L} (V_{GS} - V_{TH})}$$

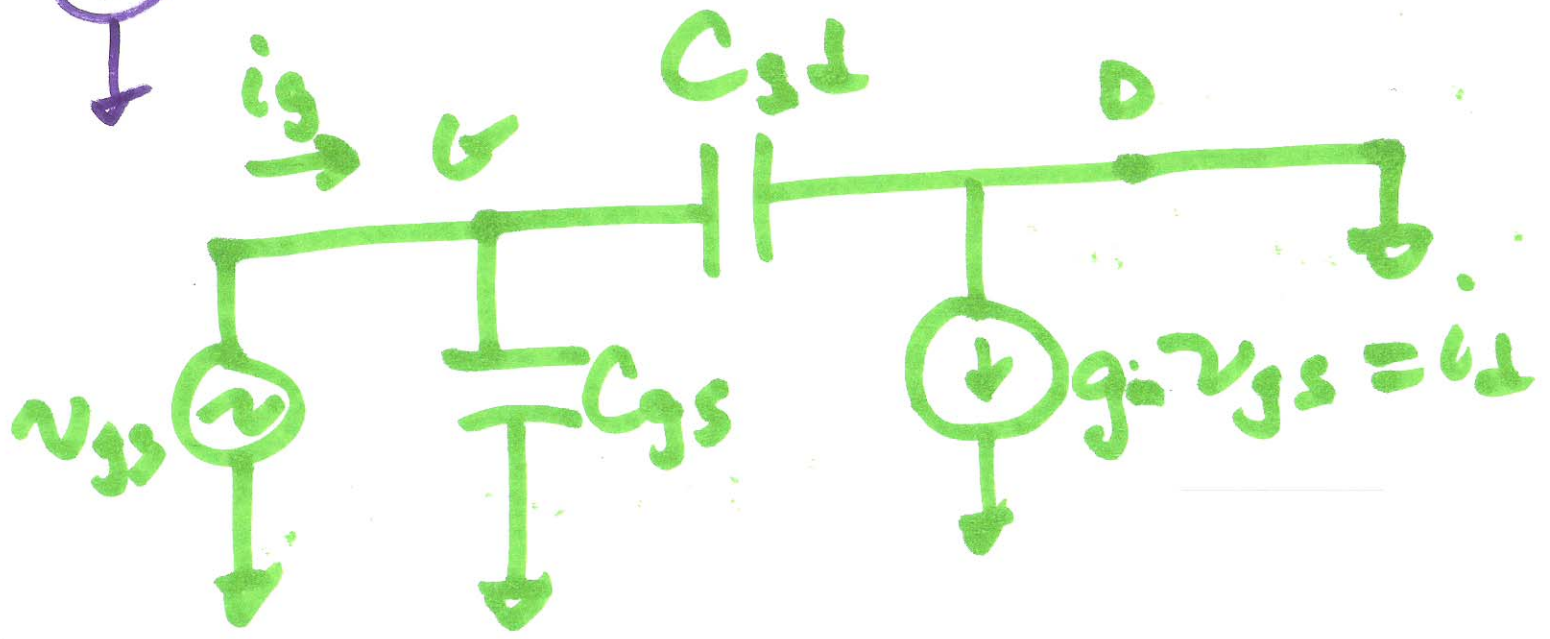
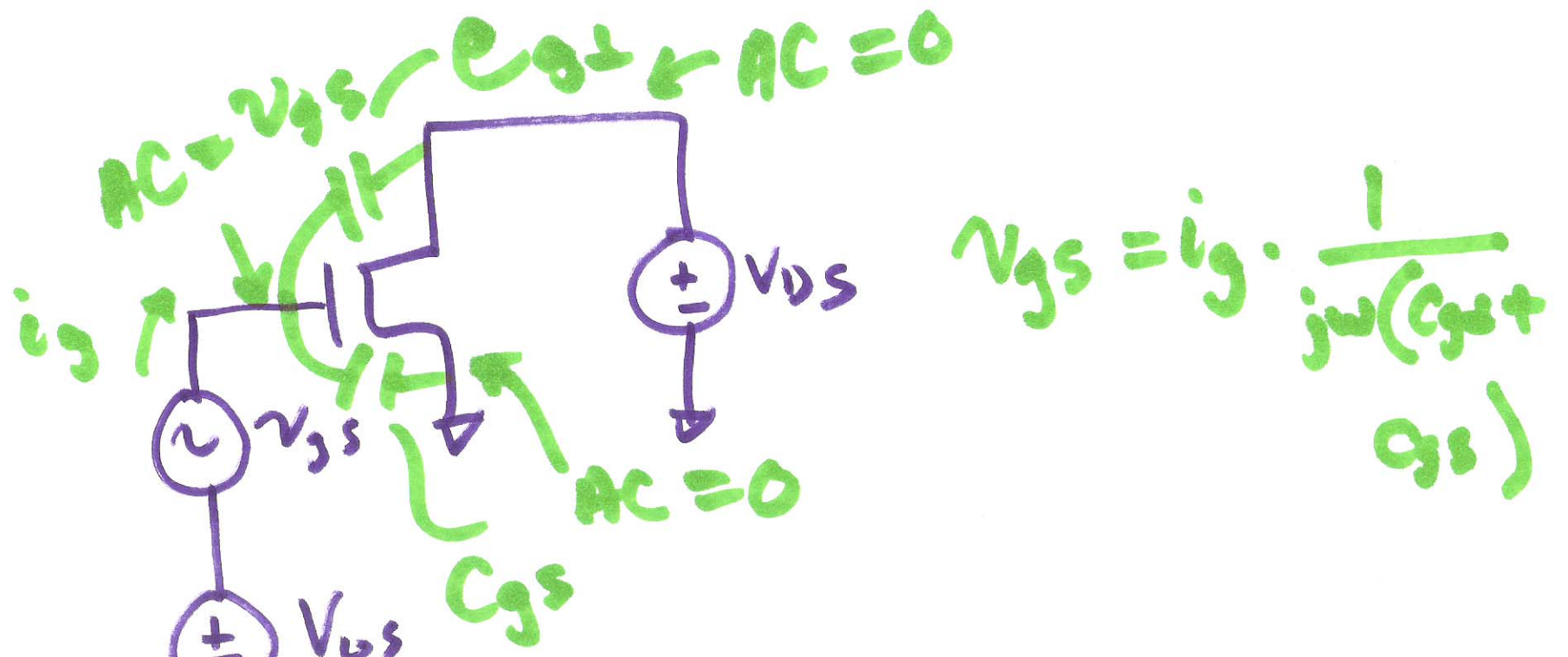
$$= \frac{K_P \cdot W}{L} (V_{GS} - V_{TH})$$

$$\lambda \frac{K_P W}{2 L} (V_{GS} - V_{TH})^2$$



$$g_m r_o \propto \frac{1}{\lambda}$$

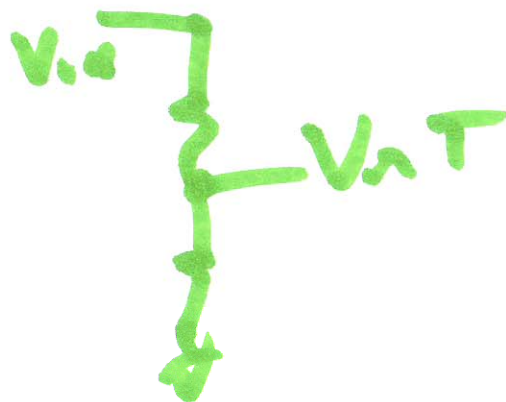




$$i_d = g_m v_{gs} = \frac{g_m \cdot i_g}{j\omega(C_{gd} + C_{gs})}$$

$$1 = \left| \frac{i_d}{i_g} \right| = \frac{g_m}{2\pi f_T (C_{gd} + C_{gs})}$$

$$\left| \frac{i_d}{i_g} \right| = 1 \quad f = f_T \leftarrow \text{MOSFET transition frequency}$$



frequency  
for an  
Amplifier  
to  
attenuation

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attenuation

$$f_T = \frac{g_m}{2\pi (C_{gd} + C_{gs})}$$

how does  $I_D$  or  $V_{GS} - V_{THN}$    
 $V_{GS, SAT}$    
 overdrive voltage

$$f_T = \frac{\sqrt{2\mu_n \frac{W}{L} I_D}}{2\pi (C_{gd} + C_{gs})} \quad I_D \uparrow \quad f_T \uparrow$$

$$= \frac{K_P \cdot \frac{W}{L} (V_{GS} - V_{THN})}{2\pi (C_{gs} + C_{gd})} \quad V_{GS} \uparrow \quad f_T \uparrow$$

$$C_{gs} \ll C_{gs} = \frac{2}{3} W \cdot L \cdot C_{ox}$$

$$K_D = \mu_n \cdot C_{ox}' \leftarrow \frac{C_{ox}}{t_{ox}}$$

$$f_T \approx \frac{\mu_n \cdot \frac{W}{L} (V_{GS} - V_{TH})}{2\pi \frac{2}{3} \cdot W \cdot L \cdot C_{ox}}$$

$$f_T \propto \frac{1}{L^2}$$

$$\begin{aligned}
 G \cdot FT &= g_m r_o f_T \\
 &= \frac{\left[ \frac{1}{2} \mu_n C_{ox} \cdot \frac{W}{L} (V_{GS} - V_{TH}) \right]^2}{2\pi \frac{2}{3} \mu_n C_{ox} \lambda \cdot \frac{W}{L} \cdot \frac{1}{2} \mu_n C_{ox} (V_{GS} - V_{TH})^2} \\
 GFT &\approx \frac{4}{L^2}
 \end{aligned}$$

15)