

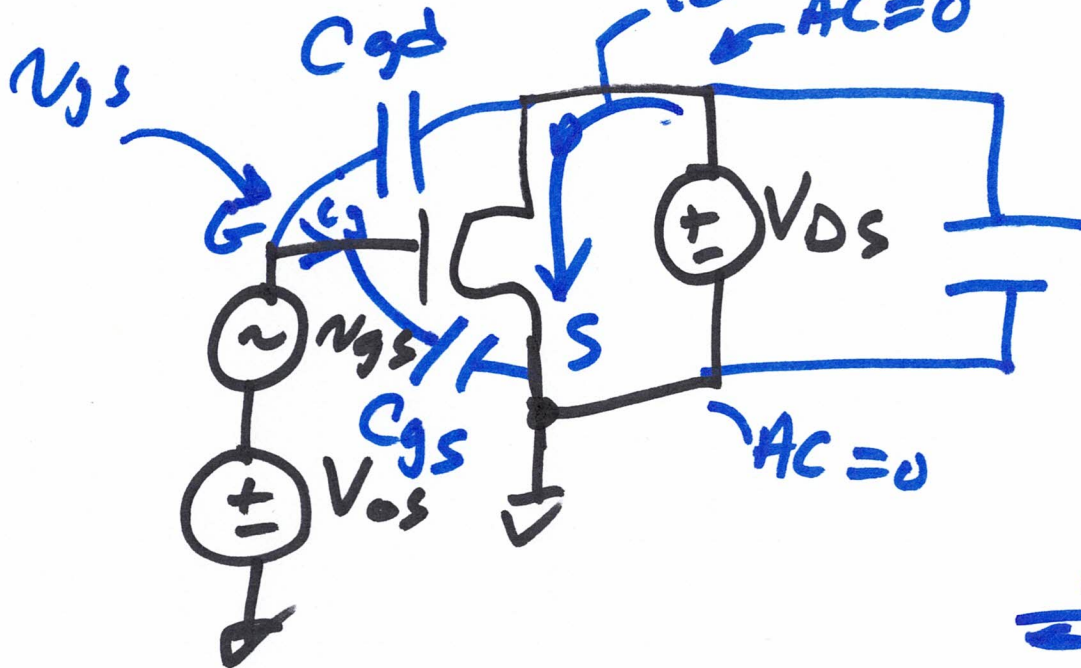
EE 420 / ECG 620

Analog IC Design

Lecture 6

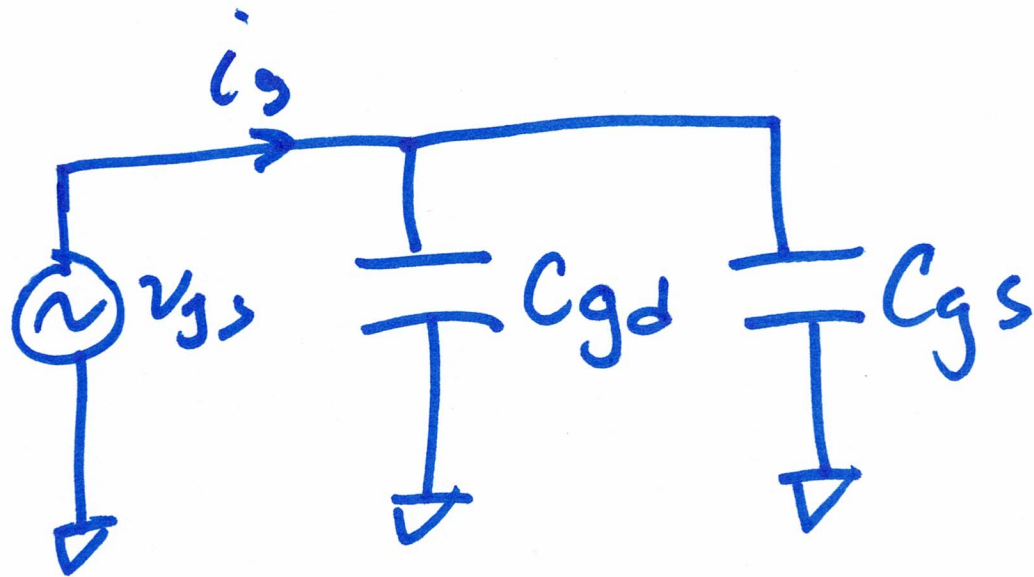
Feb. 10 2020

$$i_d = g_m v_{gs} \rightarrow v_{gs} = \frac{i_d}{g_m}$$



displacement current

Taflov



$$i_g = \frac{v_{gs}}{j\omega(C_{gd} + C_{gs})} = v_{gs} \cdot j\omega(C_{gd} + C_{gs})$$

$\frac{i_d}{g_m}$

$$\left| \frac{i_d}{i_g} \right| = \frac{g_m}{\omega \cdot (C_{gd} + C_{gs})}$$

$$1 = \left| \frac{i_d}{i_g} \right| = \frac{g_m}{2\pi f_T (C_{gd} + C_{gs})} \quad \frac{t}{\epsilon} = \frac{\epsilon \cdot A}{t}$$

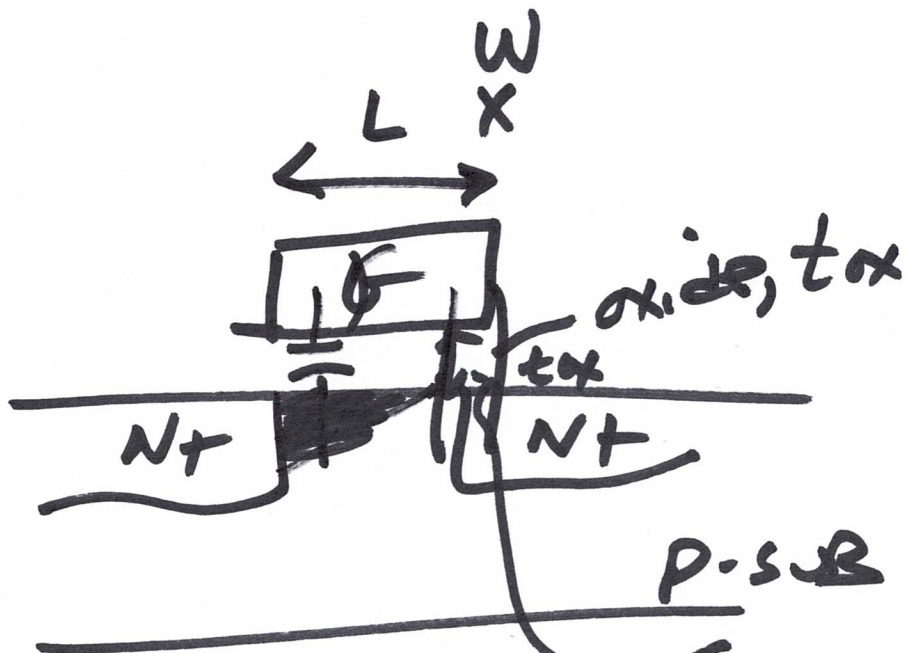
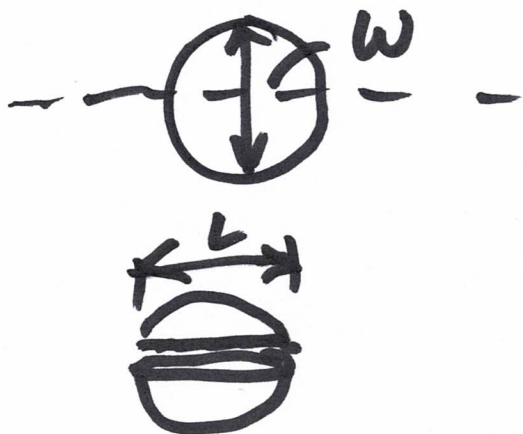
$\frac{E_{ox}}{t_{ox}}$
 $M_n \cdot C_{ox}$
 $g_m = K_P \cdot \frac{W}{L} (V_{GS} - V_{THN})$
overdrive, $V_{ovn} = V_{GS, SAT}$
 $\beta = K_P \cdot \frac{W}{L}$
 transition freq.
 Amp
 ↓
 Attenuator

$$\beta = 4nC_n \cdot \frac{W}{L} f_T = \frac{2\pi \cdot (C_{gd} + C_{gs})}{M_n \cdot C_{ox} \cdot (V_{GS} - V_{THN}) \cdot \frac{W}{L}}$$

$$f_T \approx \frac{2/3 C_{ox}}{2\pi \cdot 2/3 W \cdot L \cdot C_{ox}}$$

$C_{gs} \gg C_{gd}$

3)



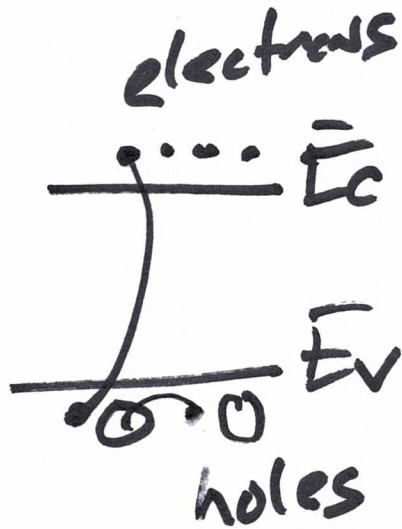
$$C_{ox} = \frac{t_{ox}}{t_{ox}} \cdot W \cdot L$$

C_{ox}

$$t_{gd} =$$

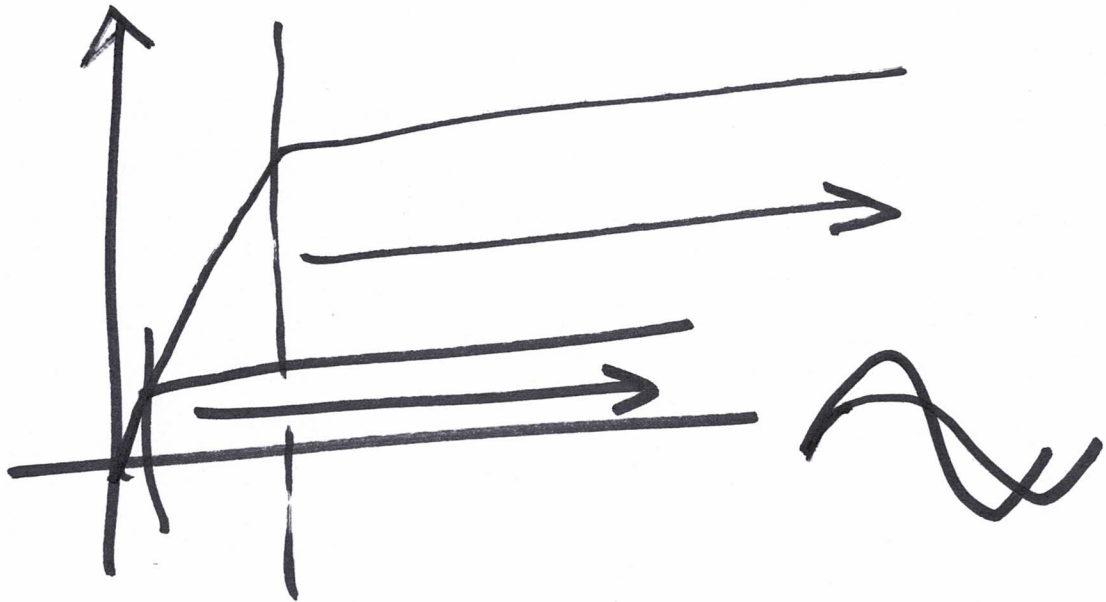
$$f_T \approx$$

$$\frac{4n \cdot (V_{GS} - V_{THN})}{2\pi \cdot \frac{2}{3} \cdot L^2}$$



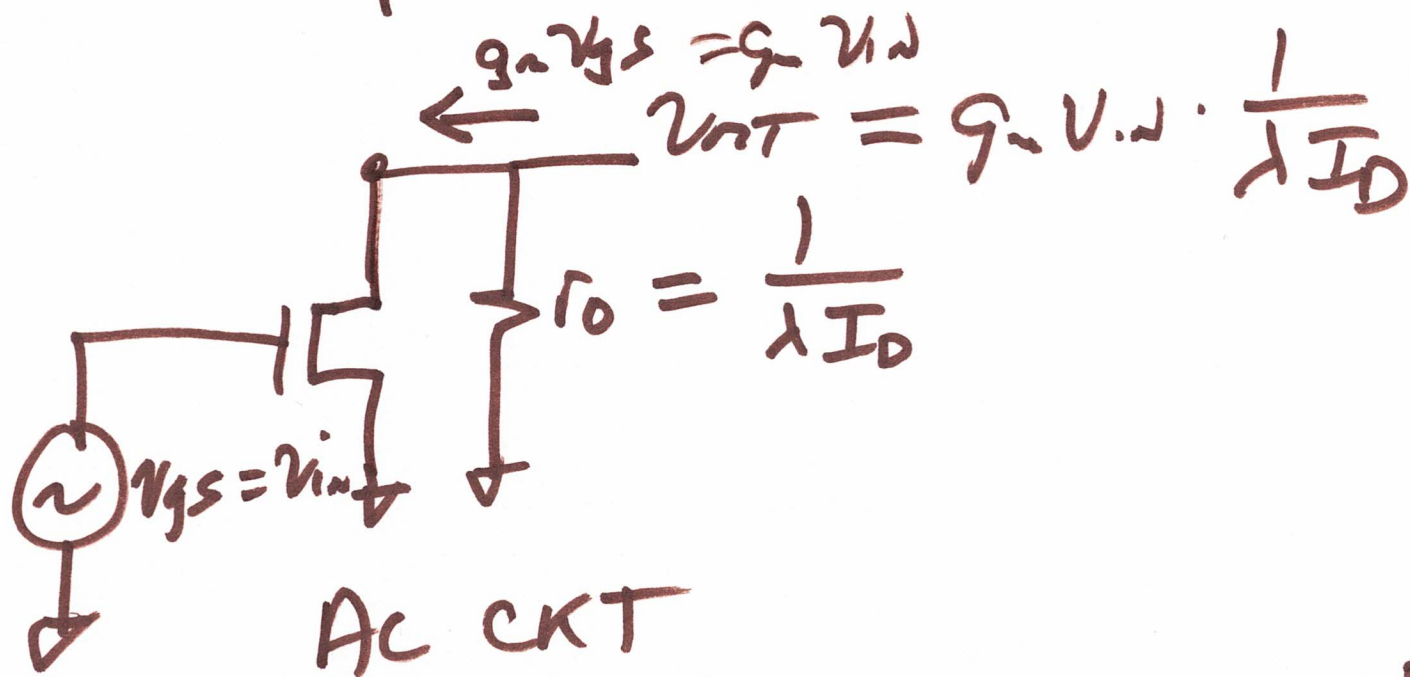
$$V_{GS} - V_{THN} = V_{OS, SAT} = V_{OVN}$$

$W \rightarrow$ selected
based current
drive needed



5)

OPEN-CKT GAIN



Open ckt gain = $\left| \frac{v_{out}}{v_{in}} \right| = g_m \cdot \frac{1}{\lambda I_D} = \frac{\sqrt{2k_p \cdot \frac{W}{L} \cdot I_D}}{\lambda I_D}$

$\rightarrow g_m r_o = \frac{\sqrt{2k_p \cdot \frac{W}{L}}}{\lambda \sqrt{I_D}}$

low I_D
 $g_m r_o \nearrow$

Figure of MERIT

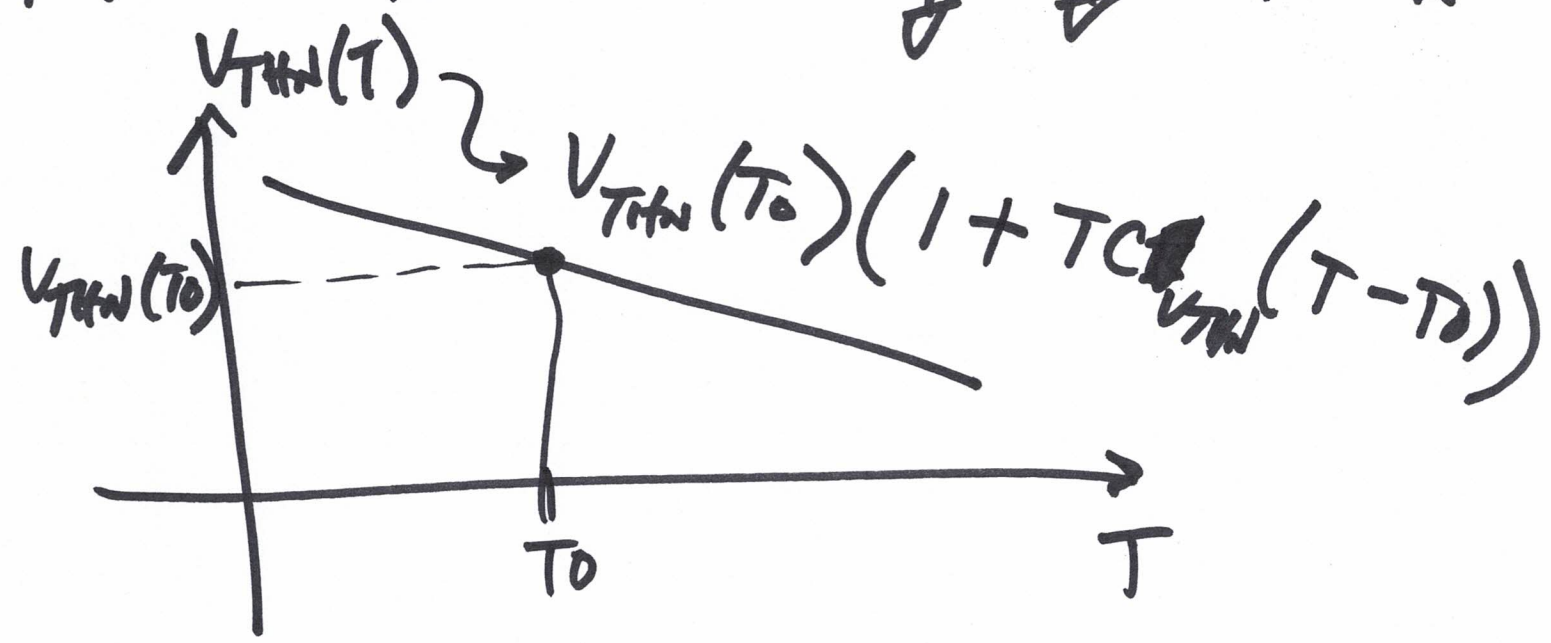
GAIN · FT (product)



Temperature behavior



4



$\mu \downarrow T \uparrow$

$V_{THN} \downarrow T \uparrow$

$$I_D = \frac{\mu_n \cdot C_{ox}}{2} \cdot \frac{W}{L} (V_{GS} - V_{THN})^2$$