

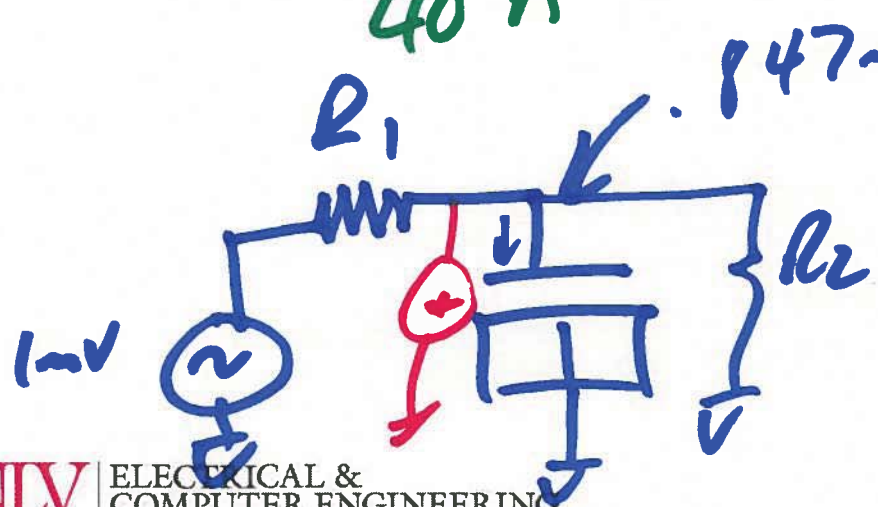
EE 421 / ECG 621

Digital IC Design

Lecture 12 OCT. 3, 2018

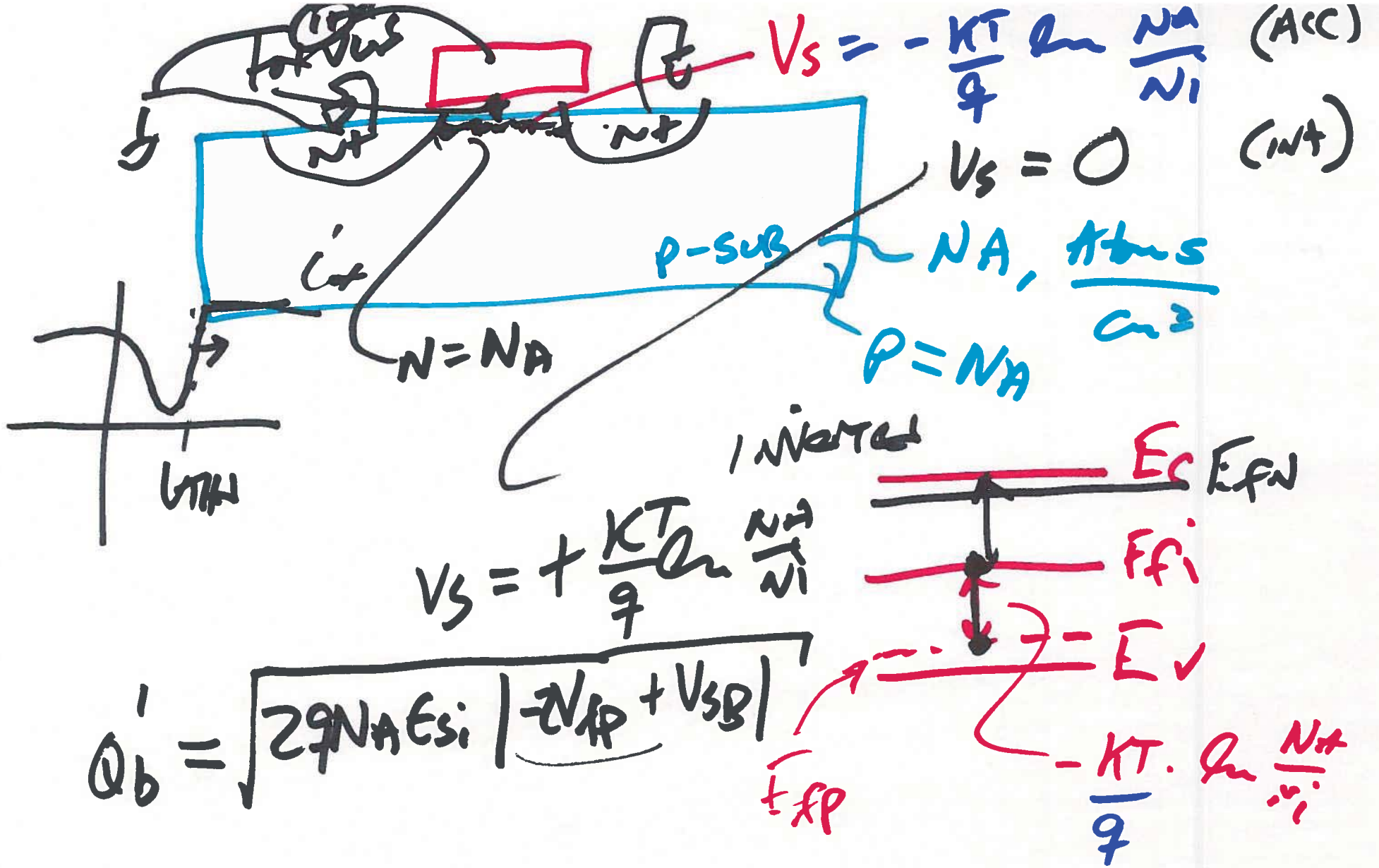
$$C_{ox}' = \frac{\epsilon_0 \cdot \epsilon_r}{t_{ox}} = \frac{3.45 \text{ aF}/\mu\text{m}}{1\mu\text{m}} = \frac{3.45 \text{ aF}}{\mu\text{m}^2}$$

$$40 \text{ \AA} = 40 \times 10^{-10} \text{ m} = 4 \text{ nm} = 0.004 \mu\text{m}$$



$$0.847 = 1 \cdot \frac{R_2}{R_1 + R_2}$$

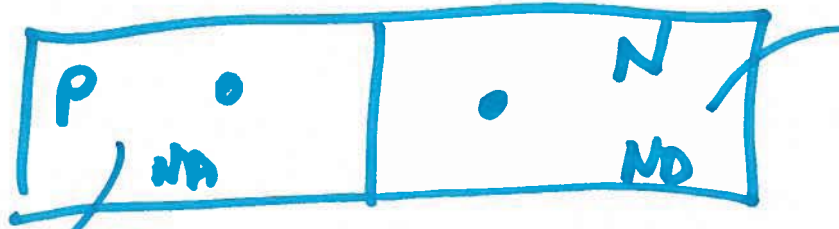
1)



2)

CONTACT potentials

-Dt



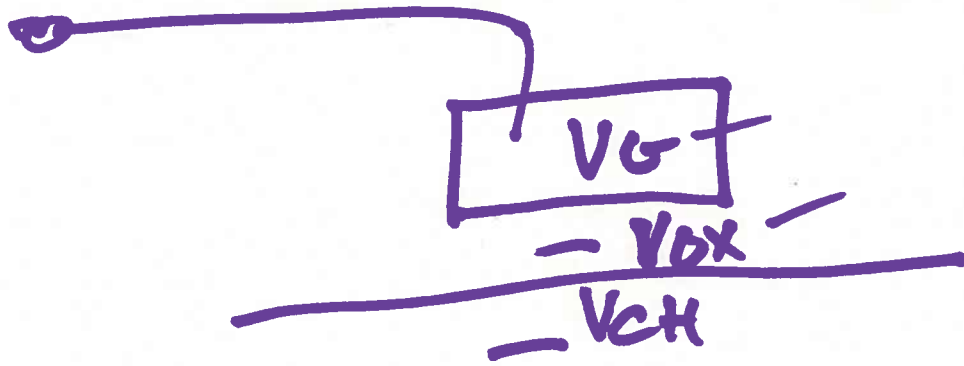
$$\frac{KT}{q} \ln \frac{ND}{ni}$$

$$-\frac{KT}{q} \ln \frac{NA}{ni} = \frac{KT}{q} \ln \frac{ni}{NA}$$

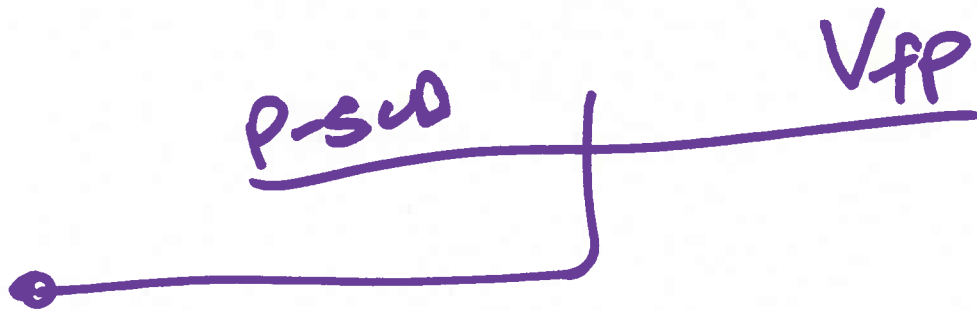
$$\frac{KT}{q} \ln \frac{ND}{ni} - \frac{KT}{q} \ln \frac{ni}{NA}$$

$$\text{contact potential} = \frac{KT}{q} \ln \frac{NDNA}{ni^2}$$

3)



$$\frac{KT}{q} \ln \frac{N_D, \text{poly}}{N_i}$$

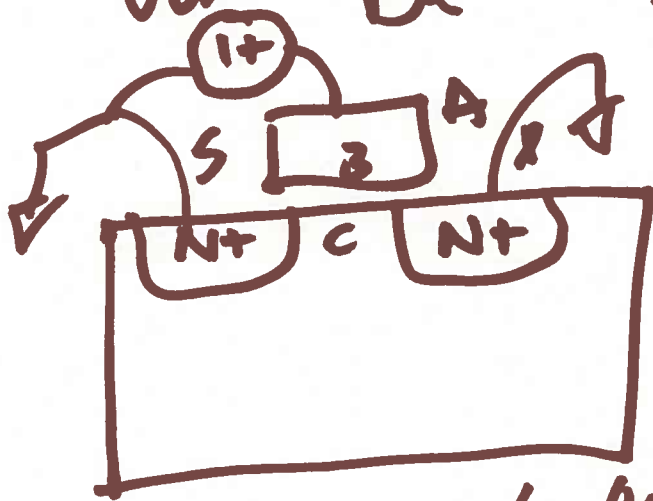


$$V_G - V_{OX} + V_{OX} - V_{CH} + V_{CH} - V_{FP}$$

Contact potential = $V_G - V_{FP} = V_{ms}$

4)

$V_{GS} = V_{DD}$ Deriving threshold voltage



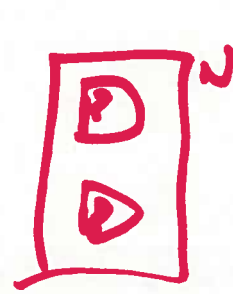
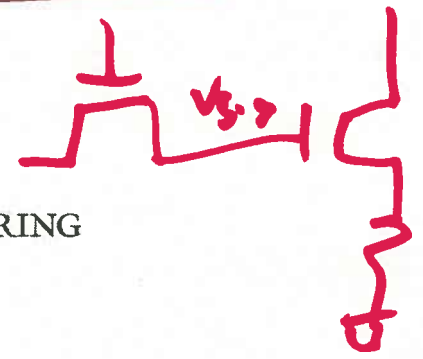
$$V_{BC} = \frac{Q'_b}{C_{ox}}$$



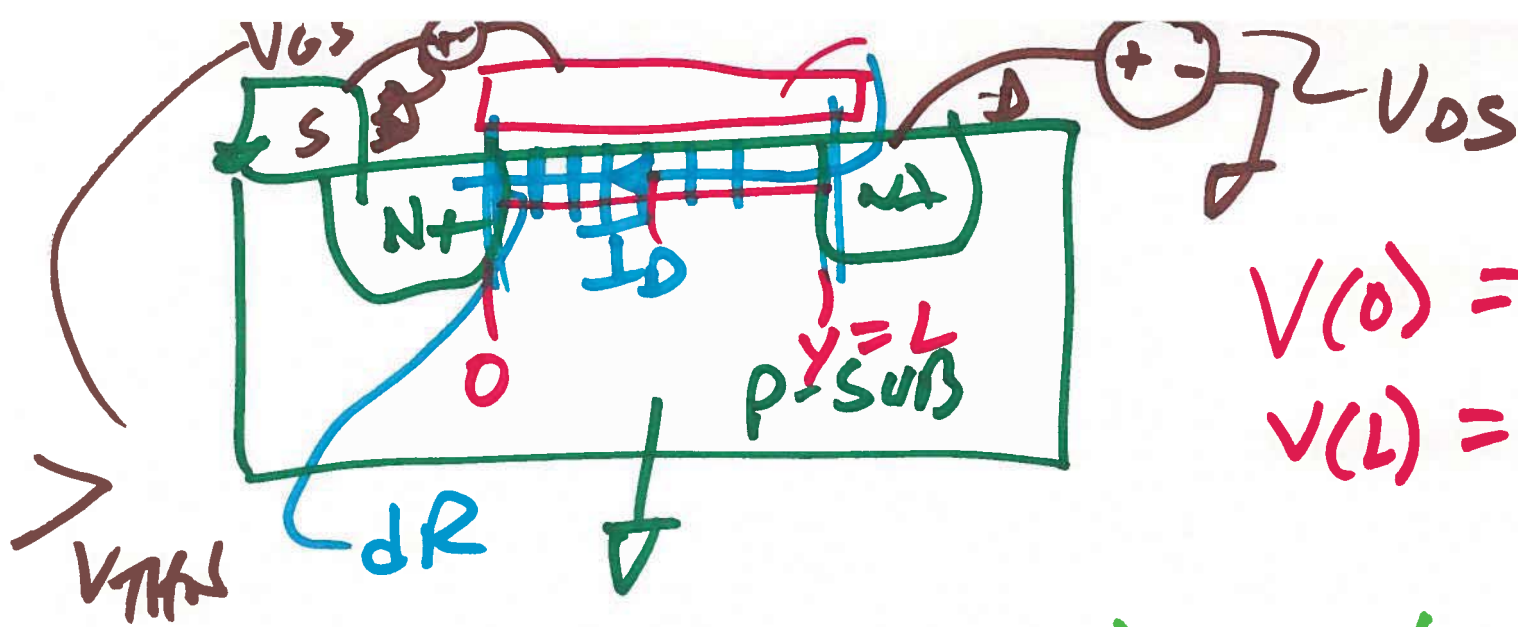
I_D vs. V_{DS}

$$V_B = \frac{Q'_b - Q'_{ss}}{C_{ox}} - 2V_{FP}$$

$$V_{THNO} = \frac{Q'_b - Q'_{ss}}{C_{ox}} - 2V_{FP} - V_{ms}$$



5)



$$V(0) = 0$$

$$V(L) = V_{DS}$$

$$\int_0^L I_D \cdot dR (V_{GS} - V(y)) \cdot C'_{ox} = Q'_{CH}$$

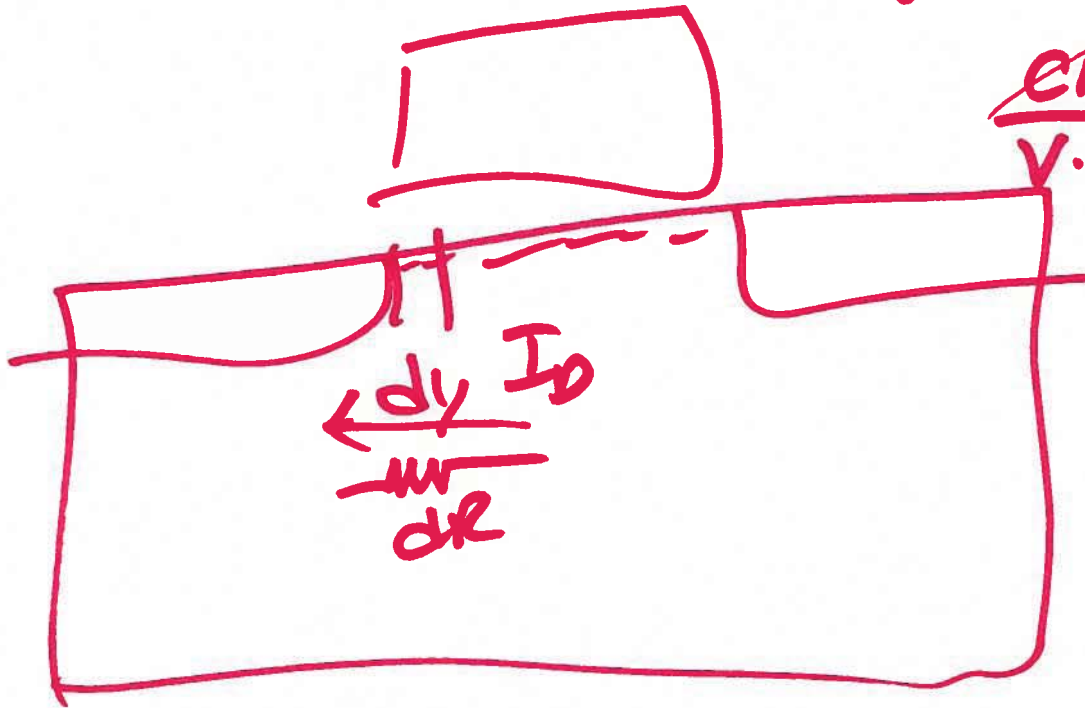
Charge AVAILABLE to conduct current $C'_{ox} \cdot V_{THN} = Q'_b$

$$Q'_I = Q'_{CH} - Q'_b$$

$$= C'_{ox} (V_{GS} - V(y) - V_{THN})$$

6)

$$dR = \frac{dy}{w} \cdot \frac{1}{\mu_n \cdot Q_I'(y)}$$



$$\frac{\text{EM}^2}{\text{V.S}} \cdot \frac{\text{Coloms}}{\text{cm}^2}$$

$$\frac{1}{\frac{\text{Coloms}}{\text{V.S}}}$$

$$\frac{\text{V}}{\text{Coloms/S}} = \frac{\text{V}}{\text{I}} = R = R$$

$$dV(y) = \frac{I_D \cdot dy}{w \cdot \mu_n \cdot Q_I'$$

$$Q_I' = C_{ox} (V_{GS} - V_{TH}) - \frac{I_D}{\mu_n}$$

7)

$$\int_0^{V_{DS}} dV(Y) \cdot W \cdot \mu_n \cdot C_{ox}' (V_{GS} - V(Y) - V_{THN}) = \int_0^L I \, dy$$

$$V_{GS} \geq V_{THN}$$

$$K_{PN} = \mu_n \cdot C_{ox}' \Rightarrow \beta_n = k_{PN} \cdot \frac{W}{L} = \mu_n \cdot C_{ox}' \cdot \frac{W}{L}$$

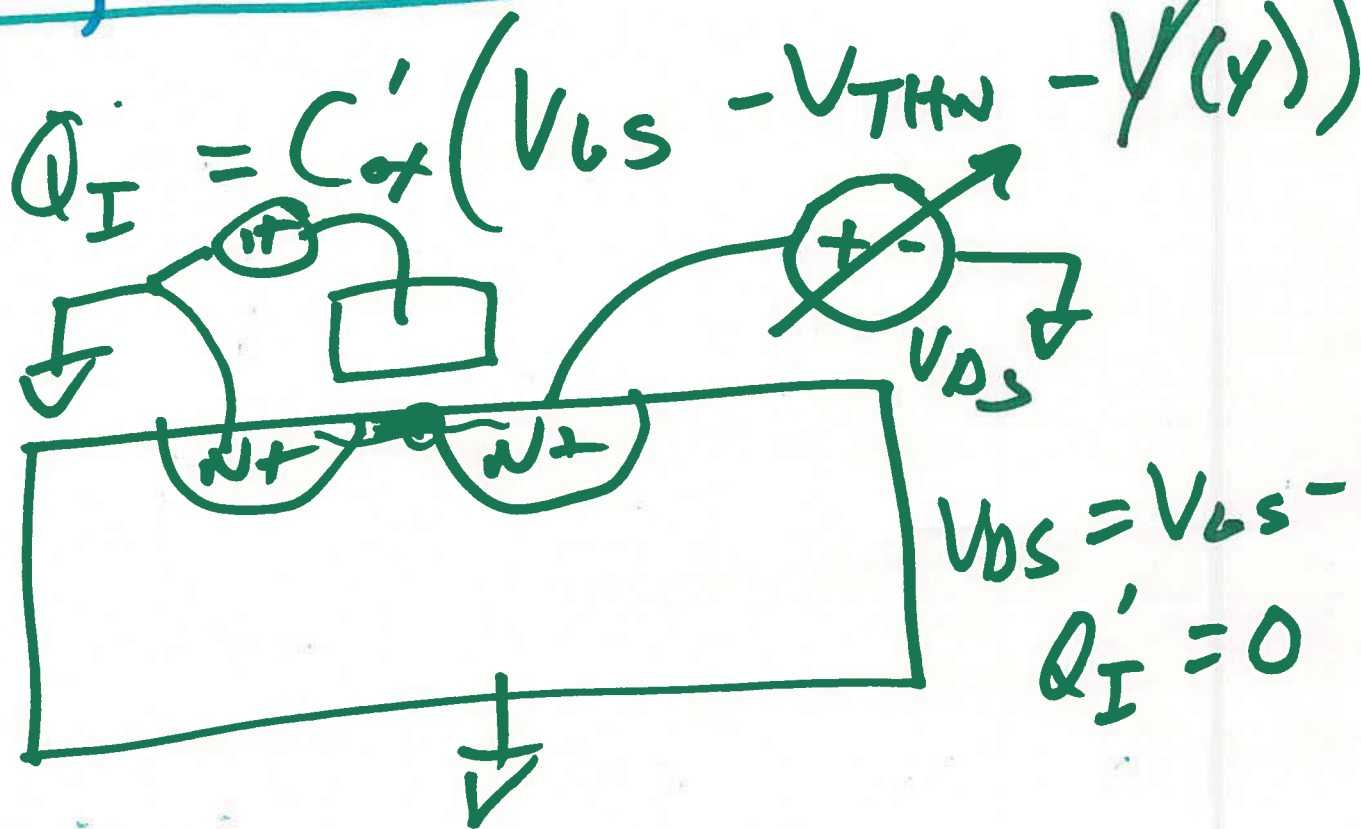
$$I \cdot L \cdot \cancel{\beta_n} = W \cdot \mu_n \cdot C_{ox}' \left[\int_0^{V_{GS}} V_{GS} \cdot dV(Y) - \int_0^{V_{GS}} V(Y) \cdot dV(Y) \right]$$

$$I \cdot L \cdot \cancel{\beta_n} = W \mu_n \left[V_{GS} \cdot V_{GS} - V_{THN} \cdot V_{GS} - \frac{1}{2} V_{GS}^2 \right]$$

Triode $I_D = \frac{W}{L} \cdot \mu_n \cdot C_{ox} \left[(V_{GS} - V_{THN}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$

$V_{DS} \leq V_{GS} - V_{THN}$, $V_{GS} \geq V_{THN}$

Triode
linear
ohmic



a)

SATURATION

$$V_{DS} \geq V_{GS} - V_{THN}, \quad V_{GS} \geq V_{THN}$$

$$I_D = \frac{W}{L} \cdot \mu_n \cdot C_{ox} \left[(V_{GS} - V_{THN})(V_{DS} - V_{THN}) - \frac{1}{2}(V_{DS} - V_{THN})^2 \right]$$

$$x^2 - \frac{1}{2}x^2 = \frac{1}{2}x^2$$

$$I_D = \frac{W}{L} \cdot \mu_n \cdot C_{ox} \frac{1}{2} (V_{GS} - V_{THN})^2$$

SAT