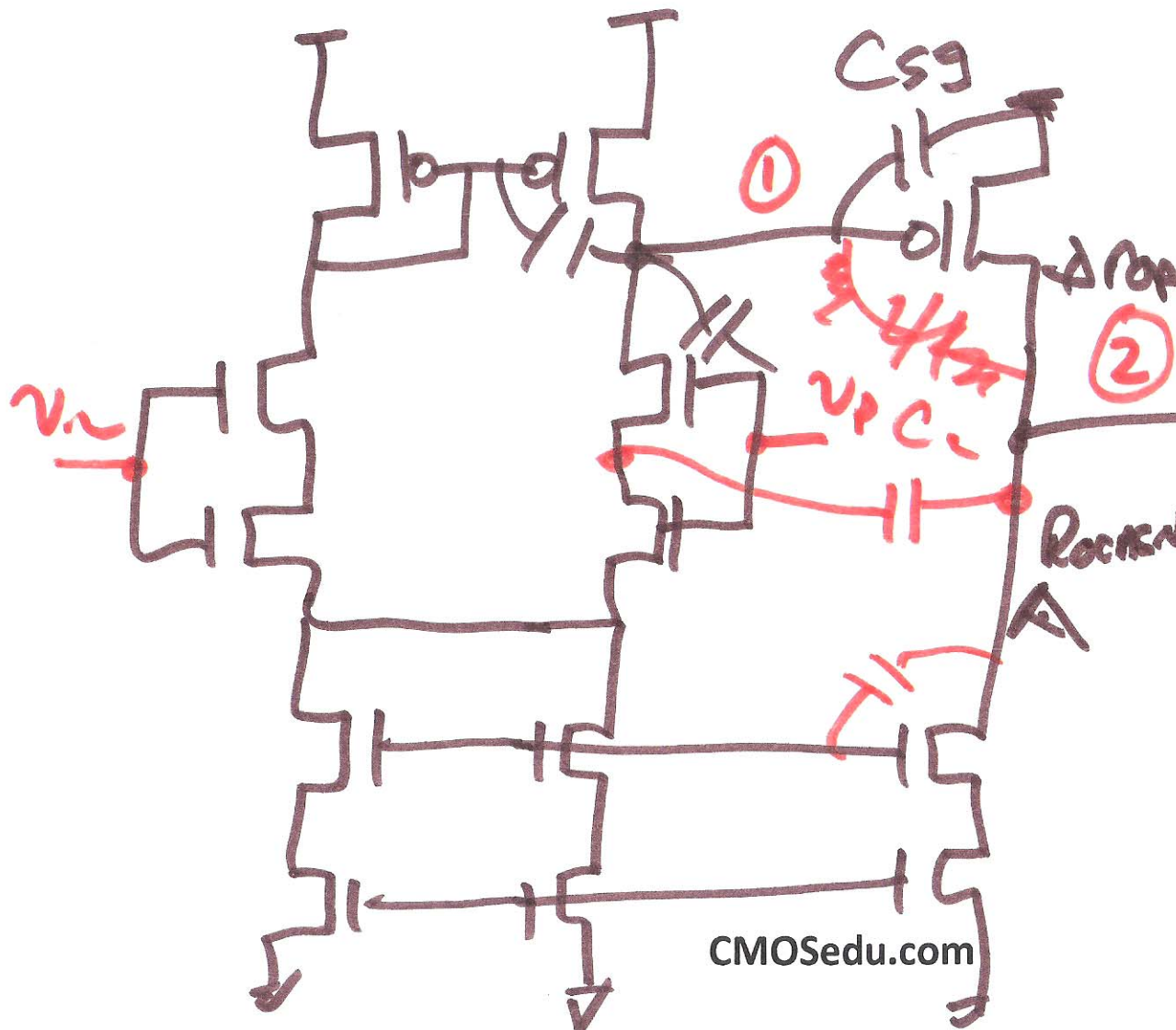


MAY 8, 2013 Lecture 77

Review for the test



$$R_1 = r_{op} \parallel r_{on}$$

$$R_2 = r_{op} \parallel R_{out} \parallel R_{in}$$

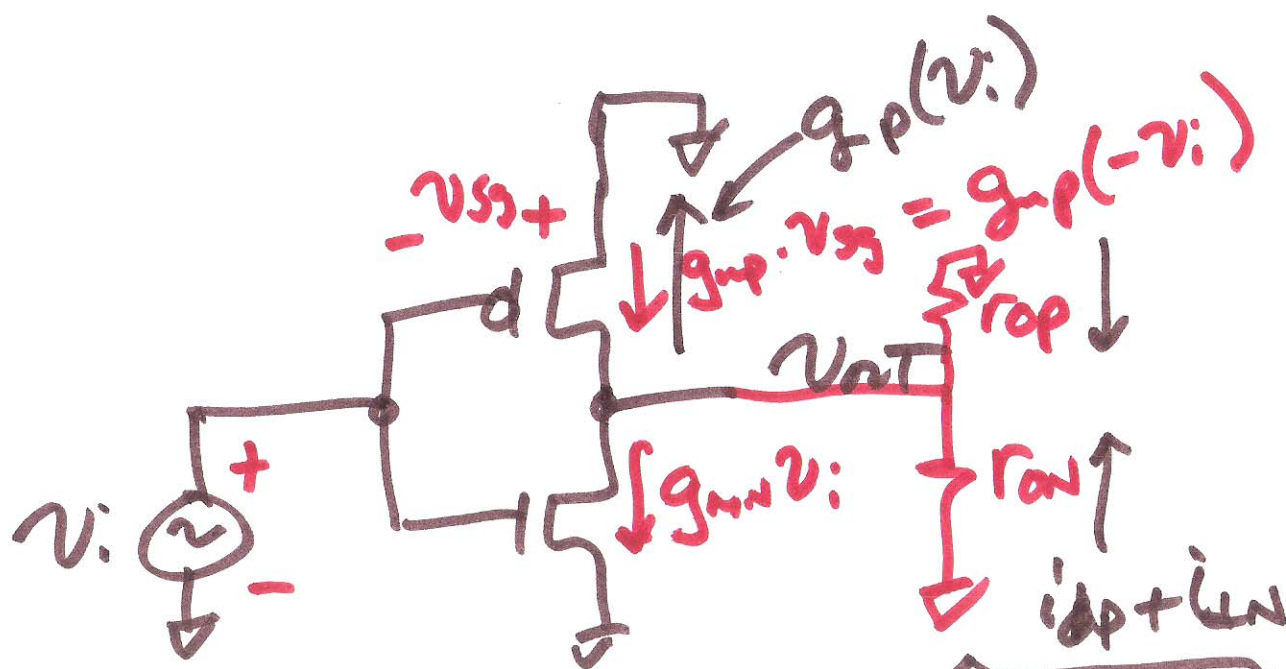
$$C_2 = C_L + C_{gd}$$

$$f_{2} = \frac{g_{m2}}{2\pi C_2}$$

$$C_1 = C_{gd} + C_{gd,n} + C_{sg}$$

$$g_{m1} = g_{m,n} \text{ (diff pair)}$$

$$g_{m2} = g_{m,p}$$



$$v_{out} = -v_i (g_{mP} + g_{mN}) \cdot r_{oN} || r_{oP}$$

$g_{-2}$

# Review for the test

Study quizzes  
H.W.

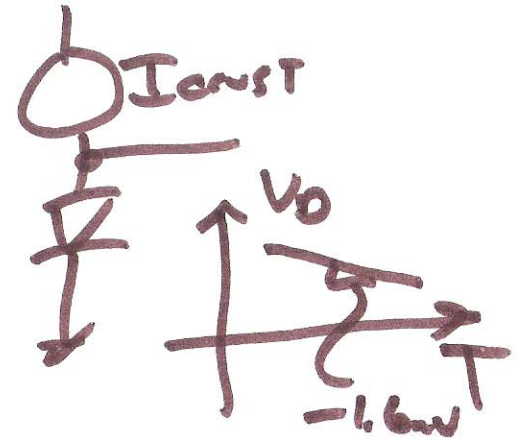
open book

EXAM  
project

Ch. 9, 20, 21, 22, 23, 24

Ch. 9 IV plots

MOS IV characteristics  
Injecting/Removing  
current



Small-signal models

$g_m, r_o$ , Ex. 9.5

Selecting  $V_{ov}, f_T, g_m$  w/L etc.

$V_{DS,SAT}, g_m r_o$

temp characteristics

3)

Ch. 20

CURRENT MIRRORS

DC operations

Matching

BIASING, B-R

\* Stability of the B-R \*

design equations  
for B-R

CASCODE

wide cascodes

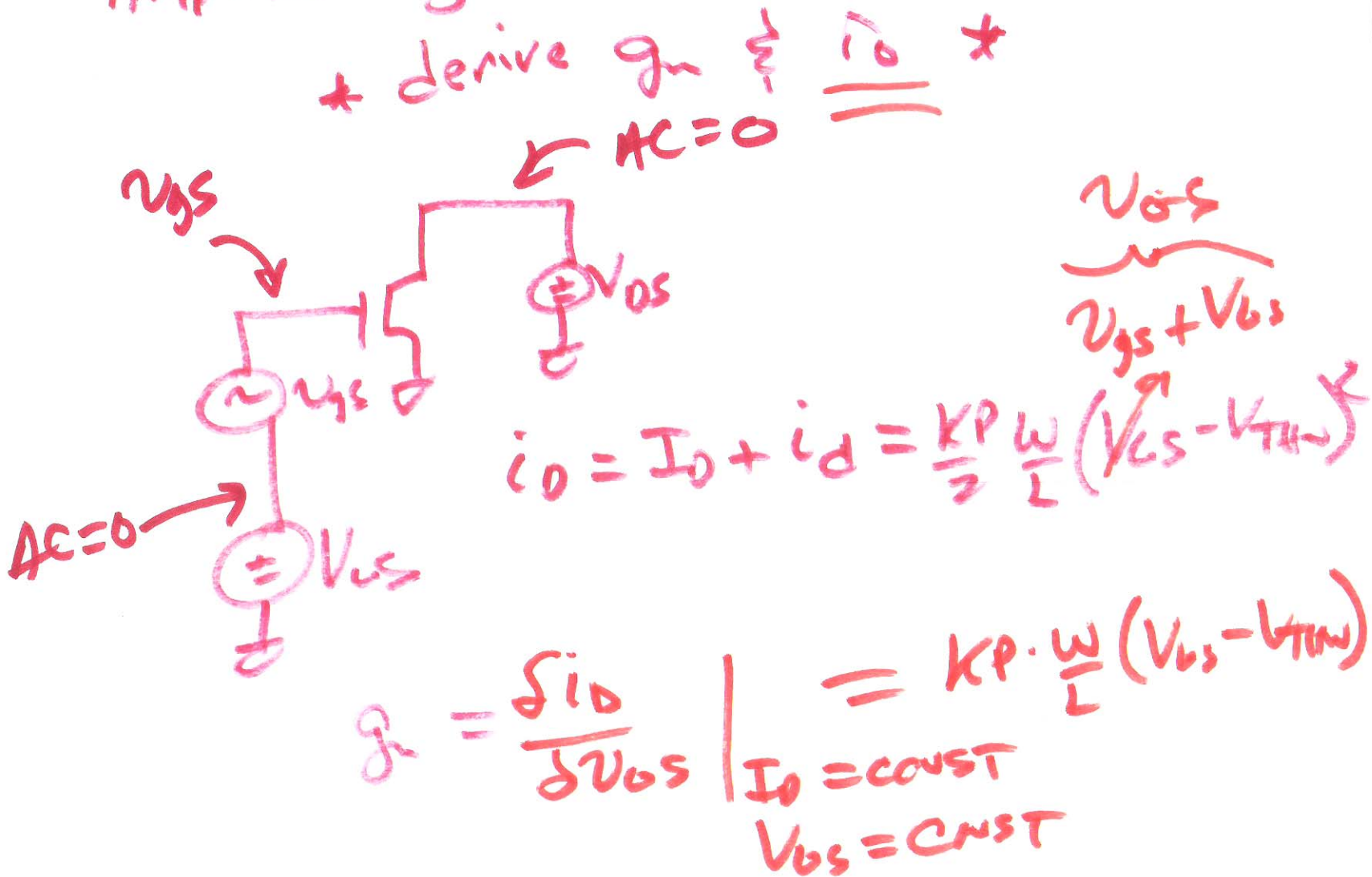
derive MWS  $\frac{1}{4} \frac{W}{L}$

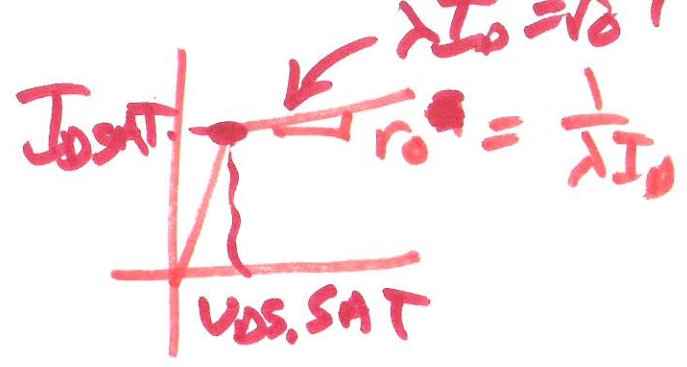
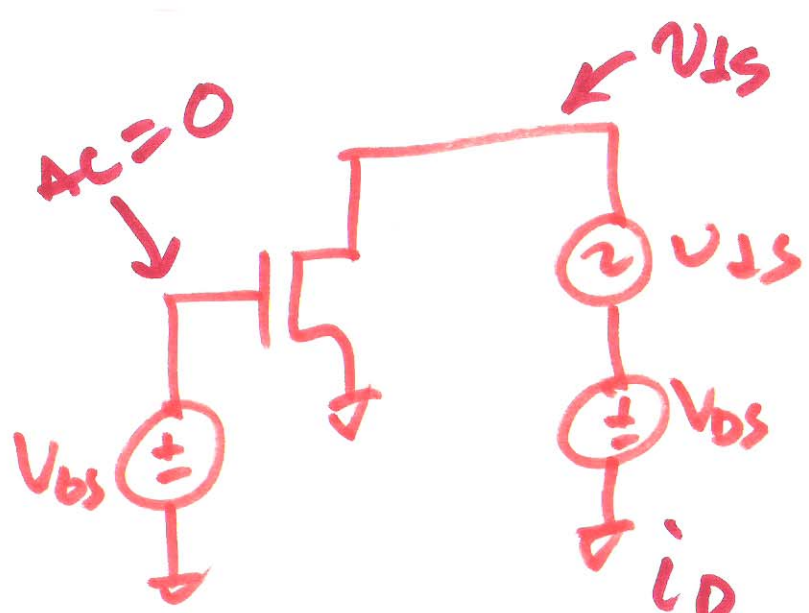
regulated cascode

Biasing CKTS.

# Amplifier gains

\* derive  $g_m \approx \frac{i_D}{v_{gs}}$  \*





$$v_{DS} = v_{DS} + v_{DS}$$

$$i_D + I_D = \frac{K_P}{2} \frac{W}{L} (V_{GS} - V_{THN})^2 (1 + \lambda v_{DS})$$

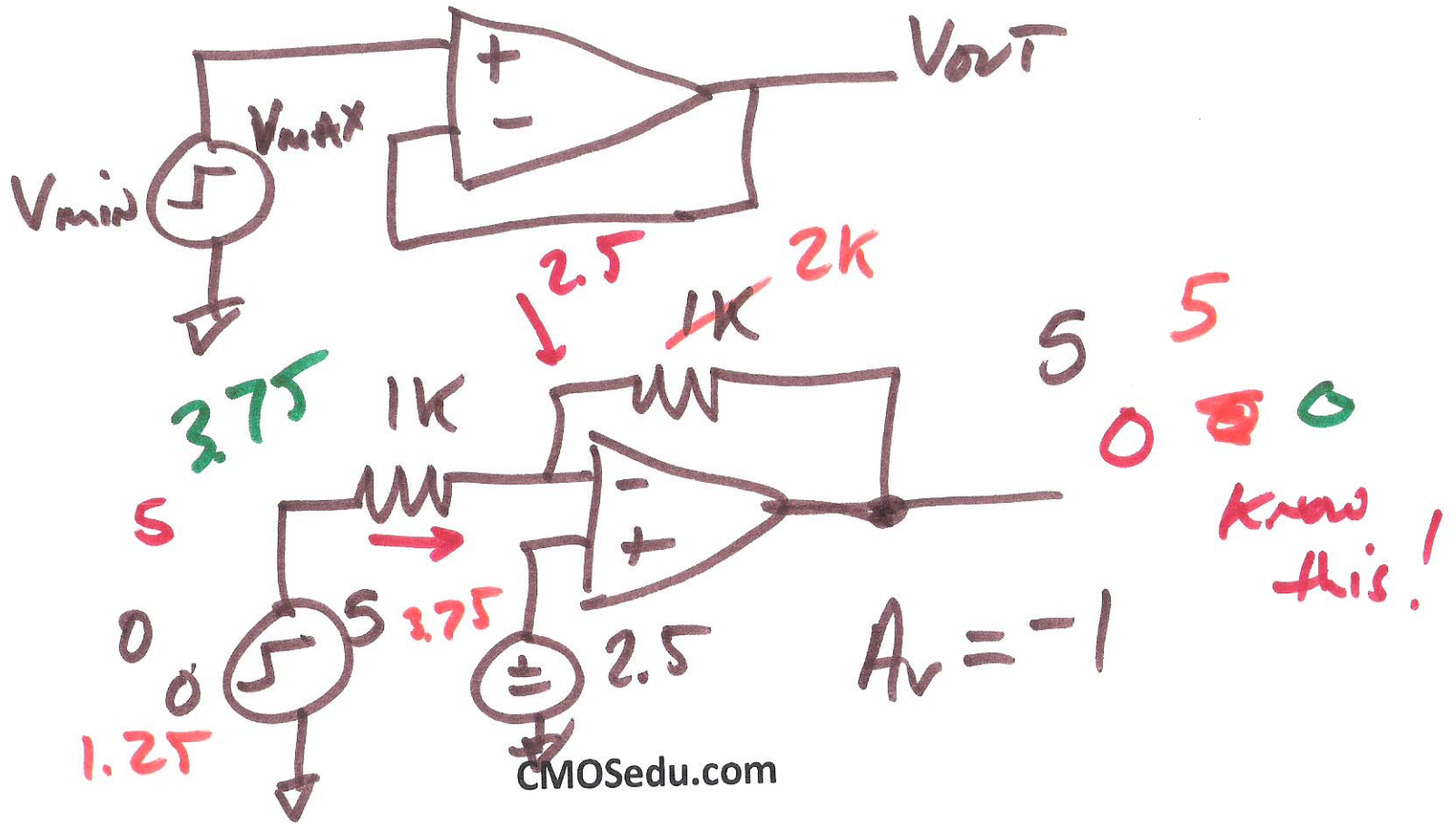
$$r_o^{-1} = \frac{\delta i_D}{\delta v_{DS}} = \frac{\frac{K_P}{2} \frac{W}{L} (V_{GS} - V_{THN})^2 \cdot \lambda \cdot \frac{\delta v_{DS}}{\delta v_{DS}}}{I_{D, SAT}}$$

$$r_o = \frac{1}{\lambda I_{D, SAT}}$$

6)

# transistor gains

diff - Amp  
SR, CMRR, AC gain  
→ INPUT CMR ←



7)

# Op-amp design

Why  $|A_{OL}| = 0dB$   
 $\angle A_{OL} = 180^\circ$ ?

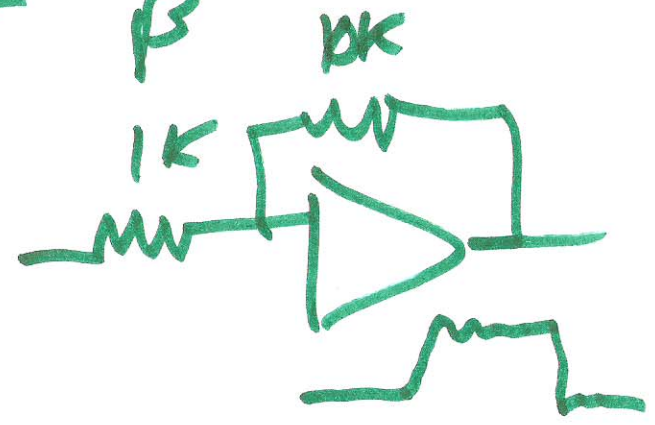
$$A_{OL} \equiv 1$$

$$A_{CL} = \frac{A_{OL}}{1 + \beta A_{OL}}$$

$$= \frac{1}{\frac{1}{A_{OL}} + \beta} = \frac{1}{\beta}$$

$A_{OL} \rightarrow \infty$

push-pull Amplifier  
OUTPUT, 24.29



for example

8)